

# EuroBeam from Greentram Software

## Typical calculations

Printed 11 Aug 2016

EuroBeam 2.90a 150001

Beam: SCI Worked Examples 4: Beam with intermediate restraints

Span: 9.0 m.

		Load name	Loading w1	Start x1	Loading w2	End x2	R1comp	R2comp
U	G	o.w.	3.0	0		L	13.50	13.50
P	G	PL1 dead	40.0	3.0			26.67	13.33
P	QA	PL1 live	60.0	3.0			40.00	20.00
P	G	PL2 dead	20.0	6.0			6.67	13.33
P	QA	PL2 live	30.0	6.0			10.00	20.00
Total load (unfactored): 177.0 kN							<b>96.83</b>	<b>80.17</b>
Dead/Permanent (unfactored): 87.0 kN							46.83	40.17
Live/Variable (unfactored): 90.0 kN							50.00	40.00
(6.10a): 211.9 kN							115.72	96.22
(6.10b): 243.6 kN							133.48	110.16

Load types: U:UDL; P:Point load; Load positions are measured in m. from R1

Load durations: G: Dead; Qx: Imposed; QA: Residential

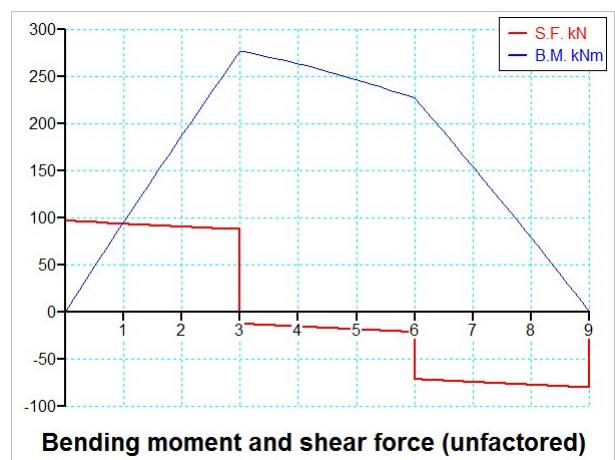
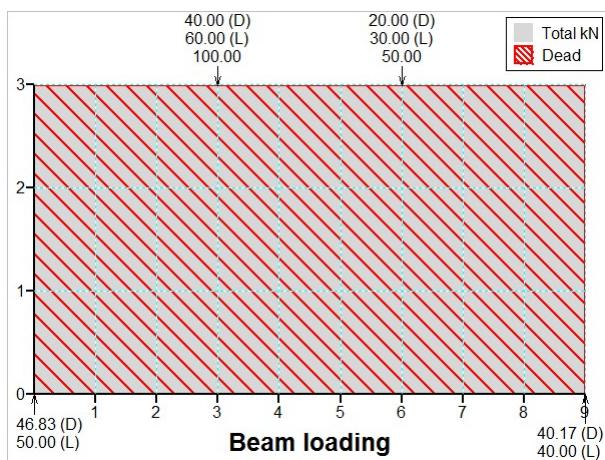
Maximum B.M. = 384 kNm (6.10b) at 3.00 m. from R1

Maximum S.F. = 133.5 kN (6.10b) at R1

Mid-span deflections: Dead:  $1,033 \times 10^8 / EI$  ( $E$  in N/mm $^2$ ,  $I$  in cm $^4$ )

Live:  $1,164 \times 10^8 / EI$

Total:  $2,197 \times 10^8 / EI$



Beam calculation to BS EN1993.1.1 using S275 steel

SECTION SIZE : 457 x 191 x 82 UKB S275 (Class 1, plastic)

D=460.0 mm B=191.3 mm t=9.9 mm T=16.0 mm  $I_y = 37,100 \text{ cm}^4$   $i_z = 4.23 \text{ cm}$   $W_{pl,y} = 1,830 \text{ cm}^3$   $W_{el,y} = 1,610 \text{ cm}^3$

Classification: Flange:  $c/t = 80.5/16.0 = 5.03 \leq 9e(8.32)$ : Class 1, plastic

EC3 Table 5.2 Web:  $c/t = 407.6/9.9 = 41.2 \leq 72e(66.6)$ : Class 1, plastic

### Shear

Design shear force,  $V_{Ed} = 133 \text{ kN}$

Shear area,  $A_v = A - 2bt_f + (t_w + 2r)t_f = 104 \times 100 - 2 \times 191 \times 16.0 + (9.90 + 2 \times 10.2) \times 16.0 = 4,763 \text{ mm}^2$  [EC3 6.2.6 (3)]

Shear resistance,  $V_{pl,Rd} = A_v \cdot (f_y / \sqrt{3}) / g_{M0} = 4,763 \times (275 / \sqrt{3}) / (1.0 \times 1000) = 756 \text{ kN} (>= 133) \text{ OK}$  [EC3 6.2.6]

Shear buckling:  $h_w / t_w = 428.0 / 9.9 = 43.23 \leq 72e(66.56)$ : check not required [EC3 6.2.6(6)]

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### Moment resistance

Design moment,  $M_{Ed} = 383.6 \text{ kNm}$

Moment resistance,  $M_{c,y,Rd} = f_y \cdot W_{pl,y} = 275 \times 1,830/1000 = 503.3 \text{ kNm OK}$

Beam is laterally restrained at 3.00m and 6.00m from R1

### Lateral-torsional buckling check

Design buckling resistance moment,  $M_{b,Rd} = c_{LT,mod} \cdot M_{c,Rd}$

$c_{LT,mod} = c_{LT}/f$  (but  $<=1/l_{LT}^2$  and  $<=1.0$ ) [Eq.6.58]

$f = 1 - 0.5(1-k_c)[1 - 2(l_{LT} - 0.8)^2]$  6.3.2.3(2)  $k_c = 1/\sqrt{C_1}$  [NA2.18]

Use buckling curve c:  $a = 0.490$  [EC3 Tables 6.3/6.4 NA 2.17]

$$c_{LT} = 1/[f_{LT} + \sqrt{(F_{LT}^2 - b l_{LT}^2)}] \quad [\text{EC3 (6.57)}]$$

$$F_{LT} = 0.5[1 + a_{LT}(l_{LT} - l_{LT,0}) + b l_{LT}^2]$$

$$l_{LT,0} = 0.4 \quad b = 0.75 \quad [\text{EC3 UK NA 2.17}]$$

$$l_{LT} = \sqrt{(f_y \cdot W_{pl,y} / M_{cr})}$$

$$M_{cr} = C_1(p^2 EI_z / L^2) \sqrt{(I_w / I_z + L^2 GI_T / p^2 EI_z)} \quad \text{SN003}$$

$$W_y = 1,830 \text{ cm}^3 \quad I_w = 0.922 \text{ dm}^6 \quad I_T = 69.2 \text{ cm}^4 \quad G = 81,000 \text{ N/mm}^2$$

Segment	$M_{Max}$	$C_1$	$k_c$	$M_{cr}$	$I_z$	$I_{LT}$	$f_{LT}$	$c_{LT}$	$c_{LT, mod}$	$M_{c,Rd}$	$M_{b,Rd}$
0.00-3.00	383.6	1.75u	0.75	1886.0	0.817	0.517	0.629	0.934	1.000	503.3	503.3 OK
3.00-6.00	383.6	1.18u	0.92	1270.2	0.817	0.629	0.705	0.868	0.903	503.3	454.2 OK
6.00-9.00	313.6	1.75u	0.76	1880.6	0.817	0.517	0.629	0.934	1.000	503.3	503.3 OK

C1 derivation: u: User-entered value

### Combined bending and shear

$V_{Ed} <= 0.5 V_{c,Rd}$  : Check for bending/shear interaction not required [EC3 6.2.8(2)]

### Web capacity at bearings

Resistance of web to transverse forces,  $F_{Rd} = f_{yw} \cdot L_{eff} \cdot t_w / g_{M1}$

$$f_{yw} = 275 \text{ N/mm}^2$$

$$L_{eff} = c_F l_y$$

$$c_F = 0.5/l_F <= 1.0$$

$$l_F = \sqrt{(l_y \cdot t_w \cdot f_{yw} / F_{cr})}$$

$$F_{cr} = 0.9k_f \cdot E \cdot (t_w^3 / h_w)$$

$$k_F = 2 + 6((S_s + c)/h_w)^2 <= 6$$

Type (c) load application assumed:

$$l_y = \min(S_s + 2t_f(1 + \sqrt{(m_1 + m_2)}), l_e + t_f\sqrt{(m_1/2 + (l_e/t_f)^2 + m_2)} \text{ or } l_e + t_f\sqrt{(m_1 + m_2)})$$

$$l_e = k_F \cdot E \cdot t_w^2 / (2 \cdot f_{yw} \cdot h_w) <= S_s + c$$

$$m_1 = f_{yf} \cdot b_f / (f_{yw} \cdot t_w) \quad m_2 = 0.02(h_w/t_f)^2 \text{ if } l_F > 0.5 \text{ else } 0.0$$

Reaction R1: 133.5 kN

Required minimum stiff bearing length,  $S_s = 0 \text{ mm}$

c (end of beam to stiff bearing) taken as 0.0

$$m_1 = 19.3 \quad m_2 = 0.00 \quad F_{cr} = 857 \text{ kN} \quad k_F = 2.00 \quad l_e = 0.00 \quad l_y = 49.73 \quad l_F = 0.397 \quad c_f = 1.00 \quad L_{eff} = 49.73$$

Resistance of web to transverse forces,  $F_{R,d} = 275 \times 49.73 \times 9.9/(1000 \times 1.0) = 135 \text{ kN OK}$

Reaction R2: 110.2 kN

Required minimum stiff bearing length,  $S_s = 0 \text{ mm}$

c (end of beam to stiff bearing) taken as 0.0

$$m_1 = 19.3 \quad m_2 = 0.00 \quad F_{cr} = 857 \text{ kN} \quad k_F = 2.00 \quad l_e = 0.00 \quad l_y = 49.73 \quad l_F = 0.397 \quad c_f = 1.00 \quad L_{eff} = 49.73$$

Resistance of web to transverse forces,  $F_{R,d} = 275 \times 49.73 \times 9.9/(1000 \times 1.0) = 135 \text{ kN OK}$

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### Deflection

$$\text{LL deflection} = 1164 \times 1\text{e}8 / (210,000 \times 37,100) = 14.9 \text{ mm } (\text{L}/602) \text{ OK}$$

$$\text{TL deflection} = 2197 \times 1\text{e}8 / (210,000 \times 37,100) = 28.2 \text{ mm } (\text{L}/319)$$

### Notes

You can add your own notes to calculations if desired